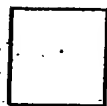


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(54) **A method of and an apparatus for automatically adjusting the characteristics of a dielectric filter**

(57) It is needed to provide a method of and an apparatus for exactly and automatically adjusting the characteristics of a dielectric filter in a short time period. The characteristic parameters (S11; S12; S21; S22) of a dielectric filter are measured, electric parameters (f1; f2; f3; k12; k23; k13) of a designed equivalent circuit of the filter are calculated with the use of characteristic parameters, characteristic adjusting portions of the dielectric filter are adjusted, while at the same time, adjustment functions indicating the variation amounts of electric parameters with respect to adjusting amounts (Zm) are calculated with the use of the electric parameters and the adjusting amounts which have been changed by the above adjustment. Then, in accordance with simultaneous equations involving adjustment functions, an adjusting amount is calculated with the use of a difference between a present electric parameter and a desired electric parameter, thereby effecting an adjustment which is for example 50%. By repeatedly conducting the above treatments, the characteristic parameters of the filter will be allowed to successively get close to the desired values.

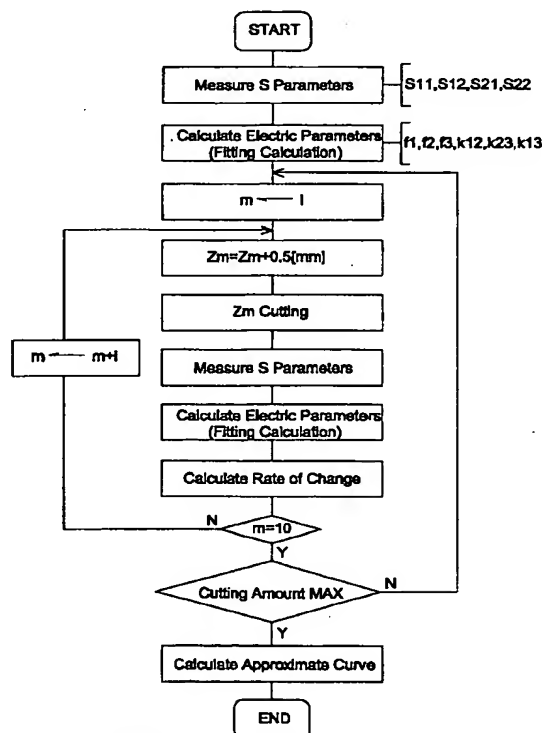


Fig. 6

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**Description****BACKGROUND OF THE INVENTION**

## 5 1. Field of the Invention

[0001] The present invention relates to a method of and an apparatus for automatically adjusting the characteristics of a dielectric filter.

## 10 2. Description of the Related Art

[0002] Typical dielectric filters are composed of electromagnetically coupled dielectric resonators. Each resonator is formed by a dielectric and electrode film on it.

15 [0003] In order to obtain a dielectric filter having desired characteristics, there has been in use a method in which some electrode portions or some dielectric portions are cut so as to be removed, alternatively some adjustment screws are driven so as to insert or remove some dielectric members or some metal members, thereby effecting a desired characteristic adjustment.

20 [0004] If physical properties of the materials forming a dielectric filter are made constant and if sizes of various portions of the dielectric filter are kept at an extremely high precision, it will be allowed to obtain substantially constant characteristics all the time. However, since there are in fact some irregularities in these characteristics, such irregularities should be taken into account when in actual design. For example, there has been in practical use a method in which when a resonance frequency is to be decided, such a resonance frequency is designed so that it is always slightly below a desired resonance frequency, and some dielectric portions are cut and removed until the resonance frequency becomes a desired resonance frequency.

25 [0005] However, with respect to a perturbation caused due to the cutting/providing or the insertion/removing of a dielectric material or an electrically conductive material in certain adjustment positions for adjusting the above-mentioned characteristics, a characteristic change of an object being adjusted is not necessarily linear. For this reason, the characteristic adjustment was carried out in accordance with the experience and a feeling of a human worker, this however results in a problem that a productivity is low and it is impossible to carry out a constantly stabilized manufacture.

30 [0006] To cope with the above problem, Japanese Patent No. 2740925 has disclosed an automation capable of automatically adjusting the characteristics of the above-discussed electronic parts. This disclosure requires that when a characteristic variation relationship is calculated with respect to an adjusting amount at portions for characteristic adjusting so as to calculate only an adjusting amount for obtaining a predetermined characteristic in accordance with the above relationship, it is necessary to eliminate a problem called defective adjustment which is caused due to a fact that the curves of characteristic variations will be different from one another corresponding to adjusting amounts of various products. For this reason, it is needed to obtain actual data by trimming the number of predetermined samples and it is also required to successively renew the trimming conditions with respect to the electronic parts of the predetermined numbers of samples, thereby dealing with an irregularity problem occurred among several lots of electronic parts and in several manufacturing processes.

35 [0007] However, with regard to a dielectric filter formed by providing a plurality of dielectric resonators and input/output combination means, there has been in use a multiple mode dielectric resonator in order that the filter may be made light in weight and compact in size. For example, when a cross-shaped dielectric column is used so as to make use of a double mode or a triple mode, some predetermined portions of the above dielectric column have to be cut off so as to adjust the resonance frequency of each resonator. However, among a plurality of resonance modes it is impossible that the resonance frequency of one resonator acting as an adjustment object may be adjusted completely independently of other resonators. For instance, if certain portions of the dielectric column are cut off, the resonance frequencies of several resonance modes will be undesirably changed at the same time. There is only a ratio difference, concerning which resonance mode receives the largest influence. For this reason, in a case when it is required to adjust the characteristics of a dielectric filter employing several triple mode resonators, it is no longer substantially possible to use a method in which a human operator is allowed to perform the adjustment while at the same time adjusting the characteristics thereof with the use of a network analyzer.

40 55 **SUMMARY OF THE INVENTION**

[0008] It is an object of the present invention to provide a method of and an apparatus for automatically and exactly adjusting the characteristics of a dielectric filter within a reduced time period.

[0009] The present invention comprises: an electric parameter extracting step including measuring characteristic

parameters of a dielectric filter whose characteristics are to be adjusted, and thus calculating electric parameters of a designed equivalent circuit of the filter with the use of the characteristic parameters; an adjustment function generating step including adjusting electric parameter adjusting portions of the dielectric filter, thus generating, with the use of the electric parameters obtained by an electric parameter extracting device and with the use of an adjusting amount, adjustment functions indicating a variation amount of the electric parameters with respect to the adjusting amount; an adjusting amount calculating step for calculating the adjusting amount, in accordance with simultaneous equations involving the adjustment functions, with the use of electric parameters obtained before the adjustment and with the use of desired electric parameters; and an adjusting step for adjusting an amount calculated in the adjusting amount calculating step, further, the electric parameter extracting step and the adjusting amount calculating step and the adjusting step are repeatedly carried out until the characteristic parameters of the dielectric filter arrive at predetermined values.

[0010] In the adjusting amount calculating step, an adjusting amount is calculated by multiplying a calculation result with a predetermined ratio, the calculation result being obtained by incorporating into the simultaneous equations involving the adjustment functions, the electric parameters obtained in the electric parameter extracting step and the desired electric parameters.

[0011] In this way, in accordance with the simultaneous equations involving adjustment functions, the characteristic parameters (S parameters) of the dielectric filter are measured, the adjusting amounts of electric parameter adjusting portions are calculated with the use of a difference between electric parameters of a designed equivalent circuit of the filter calculated from the characteristic parameters and the desired electric parameters. By repeatedly correcting the calculated adjusting amounts until the characteristic parameters of the dielectric filter arrive at predetermined values, it is possible to exactly and automatically adjust the characteristics of a dielectric filter without depending upon conventional experiences and feelings.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0012] Fig. 1 is a perspective view indicating a dielectric resonator section.

[0013] Fig. 2 provides a top plane view indicating the dielectric resonator section and a cross sectional view of the dielectric filter.

[0014] Fig. 3 is a view indicating an example showing portions for adjusting electric parameters.

[0015] Fig. 4 provides views indicating the relationships between three resonance modes and characteristic adjusting portions.

[0016] Fig. 5 is a graph indicating a variation of the electric parameters with respect to a cutting amount on certain one portion for adjusting the electric parameters.

[0017] Fig. 6 is a flow chart indicating a characteristic adjusting procedure.

[0018] Fig. 7 is a flow chart indicating a characteristic adjusting procedure.

[0019] Fig. 8 provides a top plane view and a cross sectional view indicating a dielectric filter.

[0020] Fig. 9 shows an equivalent circuit for the above dielectric filter.

[0021] Fig. 10 is used to indicate a relationship between the electric parameters forming a filter having the designed equivalent circuit and the electric parameters of a resonator unit.

[0022] Fig. 11 is a view indicating the process for converging, the resonance frequency of a dielectric filter consisting of a 6-stage resonator, into desired values of characteristic adjustment.

[0023] Fig. 12 is a schematic plan view of the system for automatically adjusting the characteristic of dielectric filters according to the present invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0024] A method of and an apparatus for automatically adjusting the characteristics of a dielectric filter, in relation to an embodiment of the present invention, will be described in the following with reference to Figs. 1 to 6.

[0025] Fig. 1 is a perspective view schematically indicating some important portions of a dielectric filter which is used as an object here for adjusting its characteristics. In Fig. 1, reference numeral 1 is used to represent a dielectric cavity within which there is integrally formed a composite dielectric column 2 consisting of two dielectric columns 2a and 2b arranged in a mutually orthogonal relationship with each other. Corresponding to each end face of each of the two dielectric columns 2a and 2b and on the central portion of each connection wall of the cavity 1, there is formed a recess portion 4a extending from the outer surface of each connection wall inwardly into a deep position of each one of the dielectric columns 2a and 2b, with an electrically conductive material 3a formed on the inner surface of each recess portion 4a. Each electrically conductive material 3a is in continuous connection with electrically conductive materials 3 formed on the outer surface of the cavity 1.

[0026] Fig. 2 illustrates an example in which an outer coupling loop and a coaxial connector are attached to the

above-mentioned multiple mode dielectric resonator, thereby forming a band pass filter consisting of a 3-stage resonator. In detail, Fig. 2A is a plane view schematically indicating a condition before an electrically conductive plate is attached on to the opening of the cavity, while Fig. 2B is a longitudinally sectional view seen from the front side thereof. On the outer surfaces of electrically conductive plates 10 and 11 covering up two openings formed on the upper and lower sides of the cavity 1, there are provided two coaxial connectors 14 and 15, while on the inner surfaces of the electrically conductive plates there are attached coupling loops 12 and 13. These coupling loops 12 and 13, as shown in Fig. 2A, are each arranged in a 45-degree relationship with respect to each dielectric column of a composite dielectric material 10. The coupling loop 12 is magnetically combined with  $TM_{110(x+y)}$  mode which is a first resonance mode, while the combination loop 13 is magnetically combined with  $TM_{110(x-y)}$  mode which is a second resonance mode. As will be related later in the present specification, a  $TM_{111}$  mode which is a second resonance mode will be generated in addition to the above first and third resonance modes, so that the first, second and third resonance modes may be combined successively, thereby obtaining a dielectric filter having the characteristics of a band pass filter consisting of a 3-stage resonator.

[0027] Fig. 3 indicates some portions for adjusting electric parameters of a triple mode dielectric resonator.

[0028] Fig. 4A indicates an electric field distribution of  $TM_{110(x+y)}$  mode which is the first resonance mode, Fig. 4B indicates an electric field distribution of  $TM_{111}$  mode which is the second resonance mode, Fig. 4C indicates an electric field distribution of  $TM_{110(x-y)}$  mode which is the third resonance mode.

[0029] In a case when using a triple mode resonator, the electric parameters include resonance frequencies  $f_1$ ,  $f_2$  and  $f_3$  of the first, second and third resonance modes, a coupling coefficient  $K_{12}$  between the first and second resonance modes, a coupling coefficient  $K_{23}$  between the second and third resonance modes, a coupling coefficient  $K_{13}$  between the first and third resonance modes. In order to adjust these electric parameters, it is preferable to select 9 or more than 9 portions for cutting as shown in Fig. 3. However, in practical use, 7 places are sufficient. For example, if a portion A1 is cut,  $f_1$  and  $f_2$  will rise and  $k_{12}$  will be increased. By cutting the portion A1, if a portion A2 is cut under a condition in which  $k_{12}$  is occurring (a condition in which the above first and second resonance modes are combined together),  $f_1$  and  $f_2$  will rise and  $k_{23}$  will be decreased. If portion A3 is cut, mainly  $f_2$  and  $f_3$  will rise and  $k_{23}$  will be increased. By cutting the portion A3, if a portion A4 is cut under a condition in which  $k_{23}$  is occurring (a condition in which the above second and third resonance modes are combined together),  $f_2$  and  $f_3$  will rise and  $k_{23}$  will be decreased. If a portion A5 is cut, mainly  $f_1$  and  $f_3$  will rise. Further, if portion A6a or A6b are cut, mainly  $f_1$  and  $f_3$  will rise and  $k_{13}$  will be increased. Under a condition in which  $k_{13}$  is occurring, if portion A7a or A7b are cut,  $f_1$  and  $f_3$  will rise and  $k_{13}$  will be decreased.

[0030] Herein after, the adjusting method of the present invention will be described. The method is performed by the system shown in Fig. 12 for example.

[0031] Adjusting machines 506 and 507 are controlled by the local computers 502 and 503 respectively. The adjusting machine includes a conveyer for bringing a filter to be adjusted into a predetermined portion wherein the filter is cut at the above-described adjusting portions, and a screw for removing the dielectric from the filter. The propagation of the screw is controlled by the local computer to remove predetermined amount of dielectric. After adjusting one filter, the conveyer moves to apply next another filter to the predetermined portion for cutting the dielectric. The adjusting machines are connected to network analyzers 506 and 507 for measuring the electrical characteristics of the filter to be adjusted. The analyzers also controlled by the local computers. The local computers 502 and 503 are further connected to a server computer 501 via local area network for example. Measured data may be forwarded from the local computer to the server computer and be processed in the server. In accordance with the result of the data processing, the local computers control the adjusting machines to further adjust the dielectric filters in the machines.

[0032] At first, the characteristic of a single dielectric filter is measured, the electric parameters of the filter is decomposed into electric parameters for resonator unit, so that a cutting amount of each adjustment portion and a changing amount of an electric parameter may be functionalized with the use of a least square method. Such kind of function may be made approximate with the use of an exponential function such as a second order function and a third order function. Among the above 9 adjustment portions shown in Fig. 3, if any one of A6a and A6b, and any one of A7a and A7b, are cut, and if the cutting amounts of the adjustment portions which are 7 in all are represented by  $Z_n$  ( $n = 1, 2, 3, 4, 5, 6, 7$ ), the following relational equations can thus exist.

[Equation 1]

[0033] About adjustment portion A1:

$$f_1 = f_{1ini} (1 + \psi_{11}(Z_1))$$

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$$f2 = f2ini (1 + \psi12(Z1))$$

5

$$f3 = f3ini (1 + \psi13(Z1))$$

$$k12 = k12ini + \psi14(Z1)$$

10

$$k23 = k23ini + \psi15(Z1)$$

$$k13 = k13ini + \psi16(Z1)$$

15

[0034] About adjustment portion A2:

$$f1 = flini (1 + \psi21(Z2))$$

20

$$f2 = f2ini (1 + \psi22(Z2))$$

25

$$f3 = f3ini (1 + \psi23(Z2))$$

$$k12 = k12ini + \psi24(Z2)$$

30

$$k23 = k23ini + \psi25(Z2)$$

$$k13 = k13ini + \psi26(Z2)$$

35

[0035] About adjustment portion A3:

$$f1 = flini (1 + \psi31(Z3))$$

40

$$f2 = f2ini (1 + \psi32(Z3))$$

45

$$f3 = f3ini (1 + \psi33(Z3))$$

$$k12 = k12ini + \psi34(Z3)$$

50

$$k23 = k23ini + \psi35(Z3)$$

$$k13 = k13ini + \psi36(Z3)$$

55

.....  
[0036] About adjustment portion A7:

$$f1 = f1ini (1 + \psi71(Z7))$$

$$f2 = f2ini (1 + \psi72(Z7))$$

$$f3 = f3ini (1 + \psi73(Z7))$$

$$k12 = k12ini + \psi74(Z7)$$

$$k23 = k23ini + \psi75(Z7)$$

$$k13 = k13ini + \psi76(Z7)$$

[0037] Here,  $f1ini$ ,  $f2ini$ ,  $f3ini$ ,  $k12ini$ ,  $k23ini$ ,  $k13ini$  are respectively initial values. Further,  $\psi_{mn}$  ( $n = 1, 2, 3, 4, 5, 6$ ,  $m = 1, 2, 3, 4, 5, 6$ ) is a function of a variation amount of a parameter with respect to a cutting amount, appearing as an exponential function such as a second order function or a third order function each passing through an origin 0.

[0038] The above adjustment functions  $\psi11, \psi12, \psi13, \dots, \psi21, \psi22, \psi23, \dots, \psi74, \psi75, \psi76$  may be obtained when the adjustment portions of the dielectric filter are being actually cut, thus may be obtained as variation amounts of the parameters with respect to the cutting amounts. The procedure for such a process is shown as a flow chart in Fig. 6. As shown in the flow chart, at first, various cutting amounts  $Z1$  to  $Z7$  of all the above portions are initialized, S parameters are measured, thereby calculating and thus obtaining the electric parameters  $f1, f2, f3, k12, k23, k13$  for realizing these S parameters, by virtue of a fitting calculation with respect to the designing of equivalent circuits. Then, an initial value 1 is incorporated into  $m$  which is an ordinal number of an adjustment portion, thus setting  $Z1$  at a cutting amount for one predetermined step. Here, a cutting amount for one step is a value which may be obtained by dividing, with a predetermined maximum step number, a maximum allowable cutting amount predetermined with respect to that cutting portion. For example, if the maximum cutting amount is set to be 5 mm and the maximum number of steps is set to be 10 steps, a cutting amount for one step will be 0.5 mm. At first, it is necessary to perform a calculation to obtain the variation amounts (variation coefficients) of electric parameters  $f1, f2, f3, k12, k23, k13$  at a time when the adjustment portion A1 of a sample has been cut by a cutting amount for one step. Next, the adjustment portion A2 is cut by a cutting amount for one step, so as to obtain the variation amounts of the above 6 electric parameters. Then, the adjustment portion A3 is cut by a cutting amount for one step, so as to obtain the above 6 parameters. From such a step onwards, in the similar manner, each of 7 adjustment portions is treated so as to obtain a variation amount for each electric parameter at a time when the adjustment portion has been cut by a cutting amount for one step. Subsequently, the adjustment portion A1 is cut again by a cutting amount (0.5 mm) for one step (by virtue of this, A1 will be changed from its initial state to another state in which 1.0 mm has been cut), thereby obtaining variation amounts of the above 6 electric parameters at this time. After that, the adjustment portion A2 is cut again by a cutting amount for one step, thereby obtaining variation amounts of the above 6 electric parameters at this time. From such a step onwards, in the similar manner, each of 7 adjustment portions is treated so as to obtain a variation amount of each electric parameter while at the same time cutting the adjustment portion by a cutting amount for one step. The above treatments are conducted successively and repeatedly until a cutting amount of each adjustment portion arrives at a predetermined maximum value, thereby obtaining a variation of each electric parameter with respect to a cutting amount at each adjustment portion. Finally, for each adjustment portion, a changing curve of each electric parameter with respect to a cutting amount may be obtained as an approximate curve by virtue of the Least Square Method. These curves are corresponding to the above functions  $\psi11, \psi12, \psi13, \dots, \psi21, \psi22, \psi23, \dots, \psi74, \psi75, \psi76$ .

[0039] Fig. 5 is used to show calculation results indicating variations of various electric parameters at the adjustment portion A1 under a condition where an allowable maximum cutting amount 7 mm has been cut at 7 steps. The horizontal axis is used to represent a cutting amount and the vertical axis is used to represent a rate of change for each electric parameter.  $F01, F02, F03$  are used to indicate the changes of the above  $f1, f2, f3$  in the form of a change rate. Further,  $k12, k23$  and  $k13$  are each indicated in the form of an absolute value. In an example shown in this figure, the adjustment functions may be indicated by the following second order functions.

$$\psi11(Z1) = (1.6721 \times 10^{-2})Z1^2 + (4.0662 \times 10^{-2})Z1$$

$$\psi_{12}(Z1) = (1.5943 \times 10^{-2})Z1^2 + (1.6339 \times 10^{-2})Z1$$

$$\psi_{13}(Z1) = (5.0085 \times 10^{-2})Z1^2 + (1.3070 \times 10^{-2})Z1$$

$$\psi_{14}(Z1) = (3.2535 \times 10^{-2})Z1^2 + (5.0863 \times 10^{-2})Z1$$

$$\psi_{15}(Z1) = (-1.2683 \times 10^{-2})Z1^2 + (2.6757 \times 10^{-2})Z1$$

$$\psi_{16}(Z1) = (1.4478 \times 10^{-2})Z1^2 + (3.0814 \times 10^{-2})Z1$$

**[0040]** In this example, by cutting the adjustment portion A1, f1 and f2 will be rising at a higher rate than f3. Further, k12 will be changed at a larger extent than k23 and k13.

**[0041]** In accordance with the above equation 1, since the electric parameters f1ini, f2ini, f3ini, k12ini, k23ini, k13ini may be calculated with the use of measurement results, if there are provided desired electric parameters f1, f2, f3, k12, k23, k13, it is possible to obtain cutting amounts Z1, Z2, Z3, Z4, Z5, Z6, Z7 which can satisfy the above parameters. However, even if several dielectric filters have been manufactured and assembled in the same manner, the characteristics of these dielectric filters can still be different more or less from one another, since there are existing common differences in size on various portions and an assembling precision may not be so satisfactory. For this reason, although a cutting operation may be performed in accordance with a cutting amount obtained by virtue of calculation, electric parameters will not vary in accordance with the above functions. Accordingly, it is necessary to perform a correction on the above functions in accordance with actual matters. Therefore, if a cutting is completed for about 50% of a necessary cutting amount calculated by the above calculation and the characteristic adjustment is performed in several stages, and if the initial values of the parameters are corrected, the variation of the electric parameters with respect to cutting amount may be properly dealt with in accordance with the predetermined functions. In more detail, the characteristics may be adjusted in the following manner.

**[0042]** At first, the electric parameters of a dielectric filter under a condition where cutting is not conducted at all, are used as initial values f1ini, f2ini, f3ini, k12ini, k23ini, k13ini. Further, the desired values of the electric parameters in a resonator unit, which may be used to obtain desired filter characteristics, are defined as f1trg, f2trg, f3trg, k12trg, k23trg, k13trg.

**[0043]** During an initial cutting treatment, since a correction amount with respect to an initial amount is not clear, it is required that the following simultaneous equations are solved, so as to calculate the cutting amounts Z1, Z2, Z3, Z4, Z5, Z6, Z7.

[Equation 2]

**[0044]**

$$f1trg = f1ini (1 + \psi_{11}(Z1) + \psi_{21}(Z2) + \psi_{31}(Z3) + \psi_{41}(Z4) + \psi_{51}(Z5) + \psi_{61}(Z6) + \psi_{71}(Z7) )$$

$$f2trg = f2ini (1 + \psi_{12}(Z1) + \psi_{22}(Z2) + \psi_{32}(Z3) + \psi_{42}(Z4) + \psi_{52}(Z5) + \psi_{62}(Z6) + \psi_{72}(Z7) )$$

$$f3trg = f3ini (1 + \psi_{13}(Z1) + \psi_{23}(Z2) + \psi_{33}(Z3) + \psi_{43}(Z4) + \psi_{53}(Z5) + \psi_{63}(Z6) + \psi_{73}(Z7) )$$

$$k12trg = k12ini + \psi_{14}(Z1) + \psi_{24}(Z2) + \psi_{34}(Z3) + \psi_{44}(Z4) + \psi_{54}(Z5) + \psi_{64}(Z6) + \psi_{74}(Z7)$$

$$k23trg = k23ini + \psi_{15}(Z1) + \psi_{25}(Z2) + \psi_{35}(Z3) + \psi_{45}(Z4) + \psi_{55}(Z5) + \psi_{65}(Z6) + \psi_{75}(Z7)$$



$$k13trg = k13ini + \psi16(Z1) + \psi26(Z2) + \psi36(Z3) + \psi46(Z4) + \psi56(Z5) + \psi66(Z6) + \psi76(Z7)$$

**[0045]** However, since there are 7 unknown letters and there are 6 equations, it is impossible to obtain these unknown letters in a simple manner. But, since a possible cutting amount is not boundless, for example, possible cutting amounts for Z1 to Z7 are all in a range of 0 mm to 6.0 mm, i.e., each having a limited range, it is required that these conditions and Zn to Z7 are obtained at the same time. Then, actual cutting amounts Z1' to Z7' may be calculated in the following.

$$Z1' = Z1 \times 0.5$$

$$Z2' = Z2 \times 0.5$$

$$Z3' = Z3 \times 0.5$$

$$Z4' = Z4 \times 0.5$$

$$Z5' = Z5 \times 0.5$$

$$Z6' = Z6 \times 0.5$$

$$Z7' = Z7 \times 0.5$$

**[0046]** The above coefficient 0.5 is called a cutting amount achievement ratio, a larger cutting amount achievement ratio (the closer it gets to 1 the better) can produce a higher speed for the adjustment. However, a run-in precision with respect to a desired value of an electric parameter will decrease. In contrast, if the cutting relaxation ratio is made small, a speed for the adjustment will become slow, but it is possible to improve the run-in precision with respect to a desired value of an electric parameter.

**[0047]** For the cutting treatments conducted at the second time onwards, after a previous cutting treatment (No.n-1) is finished, the electric parameters obtained from the characteristic parameters (S parameters) of a dielectric filter are defined to be f1new, f2new, f3new, k12new, k23new, k13new, and actually cut amounts are defined to be Z1', Z2', Z3', Z4', Z5', Z6', Z7', thereby calculating f1rev, f2rev, f3rev, k12rev, k23rev, k13rev, with the use of the following equations.

[Equation 3]

**[0048]**

$$f1rev = f1new / (1 + \psi11(Z1') + \psi21(Z2') + \psi31(Z3') + \psi41(Z4') + \psi51(Z5') + \psi61(Z6') + \psi71(Z7'))$$

$$f2rev = f2new / (1 + \psi12(Z1') + \psi22(Z2') + \psi32(Z3') + \psi42(Z4') + \psi52(Z5') + \psi62(Z6') + \psi72(Z7'))$$

$$f3rev = f3new / (1 + \psi13(Z1') + \psi23(Z2') + \psi33(Z3') + \psi43(Z4') + \psi53(Z5') + \psi63(Z6') + \psi73(Z7'))$$

$$K12rev = f12new - (\psi14(Z1') + \psi24(Z2') + \psi34(Z3') + \psi44(Z4') + \psi54(Z5') + \psi64(Z6') + \psi74(Z7'))$$

$$K23rev = k23new - (\psi15(Z1') + \psi25(Z2') + \psi35(Z3') + \psi45(Z4') + \psi55(Z5') + \psi65(Z6') + \psi75(Z7'))$$

$$K13rev = k13new - (\psi 16(Z1') + \psi 26(Z2') + \psi 36(Z3') + \psi 46(Z4') + \psi 56(Z5') + \psi 66(Z6') + \psi 76(Z7'))$$

[0049] The above [Equation 3] is an inverse calculation of the above [Equation 2], and may be used to calculate initial values which are needed to adjust a relationship between the present electric parameters and adjustment functions. Namely, in the above equations,

$$f1ini = f1rev$$

$$f2ini = f2rev$$

$$f3ini = f3rev$$

$$k12ini = k12rev$$

$$K23ini = k23rev$$

$$k13ini = k13rev$$

[0050] initial values may be corrected in the above manner. Then, the simultaneous equation of [Equation 2] is solved, so as to obtain new cutting amounts Z1, Z2, Z3, Z4, Z5, Z6, Z7. However, since these cutting amounts are absolute amounts, and since the cuttings of Z1' to Z7' are carried out at various adjustment portions, in addition, since the cutting amount relaxation ratios are set at 0.5, the actual cutting amounts at this time are as follows with respect to the adjustment portions A1 to A7.

$$(Z1 - Z1') \times 0.5$$

$$(Z2 - Z2') \times 0.5$$

$$(Z3 - Z3') \times 0.5$$

$$(Z4 - Z4') \times 0.5$$

$$(Z5 - Z5') \times 0.5$$

$$(Z6 - Z6') \times 0.5$$

$$(Z7 - Z7') \times 0.5$$

[0051] Here, one embodiment is indicated below by taking f1 as an example. For example, in a case where f1tag = 890 [MHz], f1ini = 880 [MHz], and if Z1 = 10 [mm] as a result of solving [Equation 2], and if a cutting relaxation ratio is set to be 0.5, then  $10 \times 0.5 = 5$  [mm], an actual cutting amount will be 5 [mm]. After that, if a measurement is again performed and it is found that f1 = 886 [MHz], f1new in [Equation 3] may be displaced by 886 [MHz], while Z1' to Z7' may be displaced by an actually cut amount (Z1' = 5 [mm]), thereby calculating f1rev, f2rev, f3rev, k12rev, k23rev, k13rev. Here, if f1rev = 879.5 [MHz], this may be used to replace f1ini in [Equation 2]. Then, f1tag = 890 [MHz] is

incorporated into [Equation 2] so as to obtain Z1 to Z7. If Z1 = 11 [mm], since a cutting amount at a first time will be 5 [mm], a cutting amount at a second time will be 3 [mm] because of  $11 - 5 = 6.6 \times 0.5 = 3$  [mm]. The treatments from this step onwards are conducted in similar manner.

**[0052]** Next, an entire procedure for the characteristic adjustment method is indicated by a flow chart shown in Fig. 7. At first, a network analyzer is used to measure S parameters (S11, S12, S21, S22) of a dielectric filter whose characteristics are to be adjusted. If a value thus measured is not within a desired range (under a condition where the cutting has not been conducted, such a measured value is surely within the desired range), the electric parameters (which are the electric parameters for realizing the characteristics indicating the above S parameters) corresponding to the above S parameters, may be obtained by virtue of a fitting calculation with respect to the designed equivalent circuit for the filter. If it is an initial cutting, the present electric parameters f1, f2, f3, k12, k23, k13 thus calculated, may be used as initial values f1ini, f2ini, f3ini, k12ini, k23ini, k13ini in the simultaneous equations shown in [Equation 2]. The desired parameters f1trg, f2trg, f3trg, k12trg, k23trg, k13trg of [Equation 2] should be obtained by a fitting calculation with respect to the designed equivalent circuit of the filter, in order that these desired parameters may be used as electric parameters for realizing desired S parameters. Further, the adjustment functions  $\psi_{11}$ ,  $\psi_{21}$ ,  $\psi_{31}$ ,  $\psi_{41}$ , ...,  $\psi_{76}$  are calculated in advance by virtue of the cutting of the samples. These known quantities are incorporated into [Equation 2] so as to calculate the cutting amounts Z1, Z2, Z3, Z4, Z5, Z6, Z7. Further, 50% of each of the cutting amounts are set to be actual cutting amounts Z1', Z2', Z3', Z4', Z5', Z6', Z7', and are then cut by a robot.

**[0053]** After that, S parameters are measured so as to determine whether they are within the desired ranges. If the measured parameters are not within the desired ranges, electric parameters can be calculated from the present S parameters. Next, the calculated electric parameters f1, f2, f3, k12, k23 and k13 are used as electric parameters f1new, f2new, f3new, k12new, k23new and k13new in [Equation 3], followed by incorporating the actual cutting amounts Z1', Z2', Z3', Z4', Z5', Z6', Z7', thereby solving [Equation 3] and thus calculating electric parameters f1rev, f2rev, f3rev, k12rev, k23rev, k13rev. Further, these parameters are used as f1ini, f2ini, f3ini, k12ini, k23ini, k13ini, so as to correct initial values. After that, the next cutting amounts Z1, Z2, Z3, Z4, Z5, Z6, Z7 are calculated from the above simultaneous equations of [Equation 2], thereby carrying out a predetermined cutting treatment by means of a robot, with an actual cutting amount being 50% of an amount which should be newly cut. By repeating the above treatment again and again, S parameters will be made gradually close to the desired ranges, thus completing the above treatment once the parameters enter the desired ranges.

**[0054]** Nevertheless, when differences with respect to the desired values of S parameters have become smaller than a predetermined values, further, when differences with respect to the desired values of electric parameters have become smaller than predetermined values, it is possible that the above cutting amount relaxation ratio may be made 100% so as to complete the adjustment at one stroke. Further, it is also possible that many repeated cutting treatments can make large the above cutting amount relaxation ratio, thus can shorten the total time necessary for the above adjustment, without bringing any influence to the run-in precision with respect to the desired values.

**[0055]** In the embodiment shown in the above, although an example has been given which is a dielectric filter consisting of a 3-stage resonator employing only one triple mode dielectric resonator, such an embodiment is also suitable for use in a case where a dielectric filter is constituted by using a single mode dielectric resonator. Further, it is also suitable for use in a case where a single one dielectric filter is formed by using a plurality of dielectric resonators.

**[0056]** Next, Figs. 8 to 11 are used to indicate another example where a dielectric filter having a band pass characteristic has been constituted, using two triple mode dielectric resonators and thus forming a 6-stage resonator.

**[0057]** Fig. 8 is used to provide views showing the structure of a dielectric filter, Fig. 8A is a plain view showing the filter but not including an electrically conductive plate disposed on the upper opening of the cavity, Fig. 8B is a longitudinally sectional view when seen from the front side thereof. On the two openings located on the upper and lower sides of cavities 1a and 1b, there are provided two electrically conductive plates 10 and 11. Two coaxial connectors 14a and 14b are attached to the outer surface of the electrically conductive plate 10, while two combination loops 12a and 12b are attached to the inner surface of plate. These combination loops 12a and 12b, as shown in Fig. 8A, are each arranged in a 45-degree relationship with respect to each dielectric column of the composite dielectric material 10. Combination loop 12a is magnetically combined with  $TM_{110(x+y)}$  mode, while combination loop 13a is magnetically combined with  $TM_{110(x-y)}$  mode. Similarly, combination loop 12b is magnetically combined with  $TM_{110(x+y)}$  mode, while combination loop 13b is magnetically combined with  $TM_{111(x-y)}$  mode. Similar to a case which is an embodiment described in the above, a  $TM_{111}$  mode is also generated, so as to be successively combined with a triple resonance mode. In this way, the combination loop 12a  $\rightarrow TM_{110(x+y)}$  mode  $\rightarrow TM_{111}$  mode  $\rightarrow TM_{110(x-y)}$  mode  $\rightarrow$  combination loops 13a, 13b  $\rightarrow TM_{110(x-y)}$  mode  $\rightarrow TM_{111}$  mode  $\rightarrow TM_{110(x+y)}$  mode  $\rightarrow$  combination loop 14b, may be combined successively in the above order, thereby forming a dielectric filter which has a band pass filter characteristic consisting of a 6-stage resonator.

**[0058]** An equivalent circuit designed for the above filter is shown in Fig. 9. Further, relationships between the electric parameters and the electric parameters of one resonator unit are shown in Fig. 10. As shown in Fig. 10, the designed parameters are electric parameters on an equivalent circuit designed for a filter consisting of a 6-stage resonator.

Among the above designed parameters, K12, K23, K34, K45, K56 are main coupling coefficients, while K13 and K46 are polarization and coupling coefficients for generating attenuation poles. Further, among the above parameters, the resonator unit electric parameters  $f_1$ ,  $f_2$ ,  $f_3$ ,  $k_{12}$ ,  $k_{23}$ ,  $k_{13}$  are those to be adjusted. Among the designed parameters, K01, K34, K67, K03, K47, K07, Q1 to Q6, are fixed parameters, so that they are not to be adjusted. However, in Fig. 9, K03, K47, K07 are omitted.

[0059] Similar to the case described in the above concerning a dielectric filter employing only one triple mode dielectric resonator, if the above characteristic adjustment is repeatedly carried out, the above designed parameters will get close to the desired values, thereby enabling the S parameters to be within the desired ranges. The images indicating the variations of the designed parameters F1 to F6 with the adjustment of the characteristics at this moment, are shown in Fig. 11. In this way, the resonance frequencies of each resonator as initial characteristics before cutting treatment are usually different from one another, but will be converged gradually into predetermined values step by step through the above process.

[0060] The present embodiment has taken an example which requires the adjustment of the characteristics of a dielectric filter formed by using TM mode dielectric resonator employing dielectric columns. However, in a case of a filter formed by using a TEM mode dielectric resonator with electrodes formed on dielectric block or dielectric plate, it is also possible to perform the characteristic adjustment by partially cutting off the electrodes or the dielectric portions. Further, with the TE mode dielectric resonator, it is allowed to perform the characteristic adjustment by cutting the dielectric portions.

[0061] Further, since the characteristic adjustment is effected basically by causing some kind of perturbation to the resonating system, it is also possible that said adjustment may be effected by inserting or removing a dielectric material or an electrically conductive material into or from the resonating space. Moreover, in a case where a combined adjustment is performed through a combination between the resonator and a combination means such as a combination loop, it is allowed that such an adjustment may be carried out only by adjusting the direction and deformation amount of the combination loop. In the above cases, a characteristic adjusting robot may be used to perform the above characteristics by controlling an amount of inserting/removing the dielectric material or electrically conductive material.

[0062] With the use of the present invention, in accordance with the simultaneous equations involving adjustment functions, the characteristic parameters (S parameters) of the dielectric filter are measured, the adjusting amounts of the electric parameter adjusting portions are calculated with the use of electric parameters of a designed equivalent circuit of the filter calculated from the characteristic parameters and with the use of desired electric parameters. The desired filter characteristics can be obtained simply by repeatedly correcting the calculated adjusting amount until the characteristic parameters of the dielectric filter arrive at predetermined values. For this reason, it is possible to exactly and automatically adjust the characteristics of a dielectric filter without depending upon conventional experiences and feelings.

Text for Table of Fig. 10

[0063]

- ① Designed Parameter
- ② Explanation
- ③ Resonator 1
- ④ Resonator 2
- ⑤ Frequency of the First Stage
- ⑥ Frequency of the Second Stage
- ⑦ Frequency of the Third Stage
- ⑧ Frequency of the Fourth Stage
- ⑨ Frequency of the Fifth Stage
- ⑩ Frequency of the Sixth Stage
- ⑪ Combination Coefficient between an Input Loop and the First Stage
- ⑫ Combination Coefficient between the First Stage and the Second Stage
- ⑬ Combination Coefficient between the Second Stage and the Third Stage
- ⑭ Combination Coefficient between the Third Stage and the Fourth Stage
- ⑮ Combination Coefficient by virtue of a Combination Loop
- ⑯ Combination Coefficient between the Fourth Stage and the Fifth Stage
- ⑰ Combination Coefficient between the Fifth Stage and the Sixth Stage
- ⑱ Combination Coefficient between the Sixth Stage and an Output Loop
- ⑲ Combination Coefficient between the Input Loop and the Third Stage
- ⑳ Combination Coefficient between the First Stage and the Third Stage

- (20) Combination Coefficient between the Fourth Stage and the Sixth Stage
- (21) Combination Coefficient between the Fourth Stage and the Output Loop
- (22) Combination Coefficient between the Input Loop and the Output Loop
- (23) Q of the First Stage
- (24) Q of the Second Stage
- (25) Q of the Third Stage
- (26) Q of the Fourth Stage
- (27) Q of the Fifth Stage
- (28) Q of the Sixth Stage

## Claims

1. A method of automatically adjusting the characteristics of a dielectric filter, said method comprising :

an electric parameter (S11; S12; S21; S22) extracting step including measuring characteristic parameters of a dielectric filter whose characteristics are to be adjusted, and thus calculating electric parameters (f1; f2; f3; k12; k23; k13) of a designed equivalent circuit of the filter with the use of the characteristic parameters;  
 an adjustment function generating step including adjusting electric parameter adjusting portions of said dielectric filter, thus generating, with the use of the electric parameters obtained by an electric parameter extracting means and with the use of an adjusting amount (Zm; Z1 to Z7), adjustment functions indicating a variation amount of the electric parameters with respect to the adjusting amount;  
 an adjusting amount calculating step for calculating the adjusting amount, in accordance with simultaneous equations involving the adjustment functions, with the use of electric parameters obtained before the adjustment and with the use of desired electric parameters; and  
 an adjusting step for adjusting an amount calculated in the adjusting amount calculating step, wherein the electric parameter extracting step and the adjusting amount calculating step and the adjusting step are repeatedly carried out until the characteristic parameters of the dielectric filter arrive at predetermined values.

2. The method of automatically adjusting the characteristics of a dielectric filter according to claim 1, wherein in the adjusting amount calculating step, an adjusting amount (Zm; Z1 to Z7) is calculated by multiplying a calculation result with a predetermined ratio, the calculation result being obtained by incorporating into the simultaneous equations involving the adjustment functions, the electric parameters obtained in the electric parameter extracting step and the desired electric parameters.
3. The method of automatically adjusting the characteristics of a dielectric filter according to claim 1 or 2, wherein electric parameters obtained before the adjustment, during a first time adjustment, are electric parameters obtained by the electric parameter extracting means, during adjustments from a second time adjustment onward, are electric parameters obtained by incorporating into the simultaneous equations involving the adjustment functions, the electric parameters obtained in the electric parameter extracting step after a former adjustment, and an already-adjusted amount, followed by an inverse calculation.
4. The method of automatically adjusting the characteristics of a dielectric filter according to claim 1, 2 or 3, wherein the dielectric filter is a multiple mode dielectric filter.

5. An apparatus for automatically adjusting the characteristics of a dielectric filter, said apparatus comprising:

an electric parameter (S11; S12; S21; S22) extracting means for measuring characteristic parameters of a dielectric filter whose characteristics are to be adjusted, and thus calculating electric parameters (f1; f2; f3; k12; k23; k13) of a designed equivalent circuit of the filter with the use of the characteristic parameters;  
 an adjustment function generating means for adjusting electric parameter adjusting portions of said dielectric filter, thus generating, with the use of the electric parameters obtained by an electric parameter extracting means and with the use of an adjusting amount (Zm; Z1 to Z7), adjustment functions indicating a variation amount of the electric parameters with respect to the adjusting amount;  
 an adjusting amount calculating means for calculating the adjusting amount, in accordance with simultaneous equations involving the adjustment functions, with the use of electric parameters obtained before the adjustment and with the use of desired electric parameters; and

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an adjusting means for adjusting an amount calculated by the adjusting amount calculating means,  
a control means for repeatedly conducting a treatment using the electric parameter extracting means and a  
treatment using the adjusting amount calculating means and a treatment using the adjusting means, until the  
characteristic parameters of the dielectric filter arrive at predetermined values.

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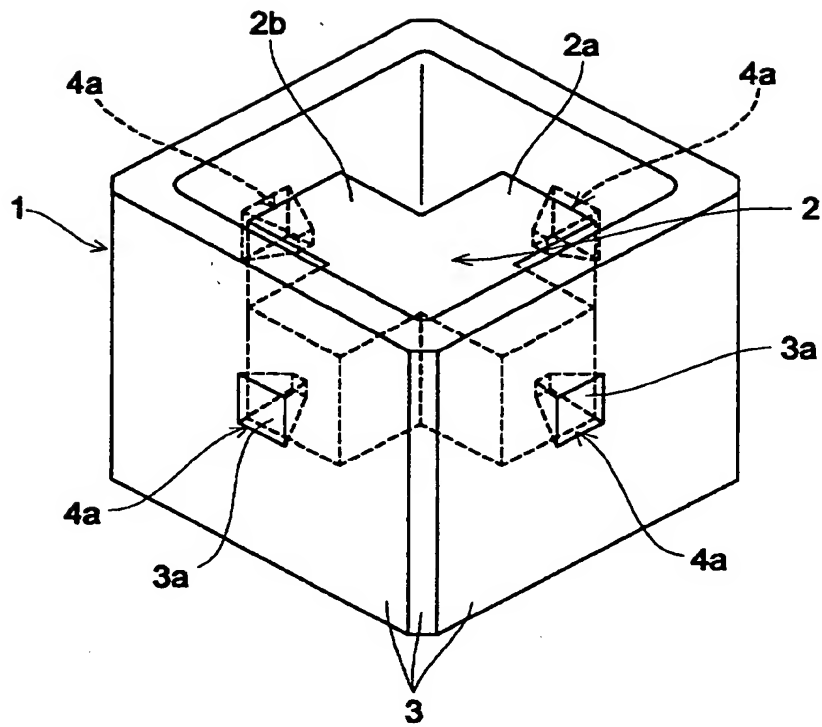


Fig. 1

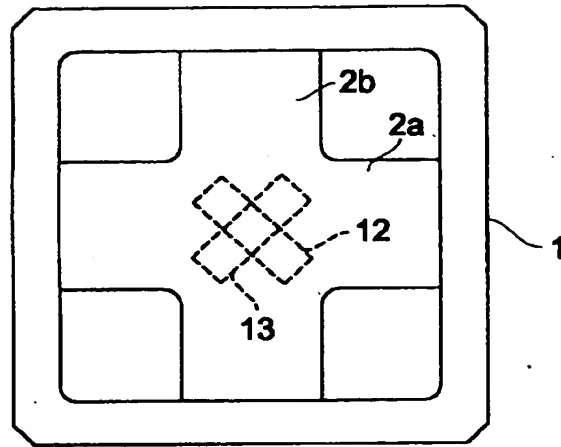


Fig. 2A

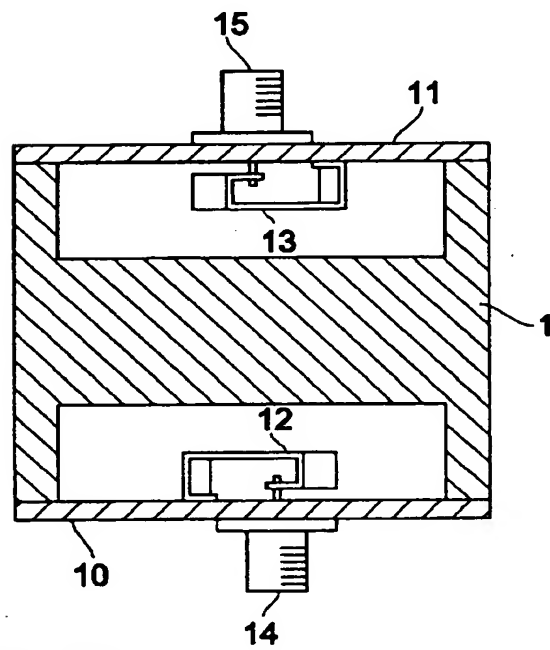


Fig. 2B



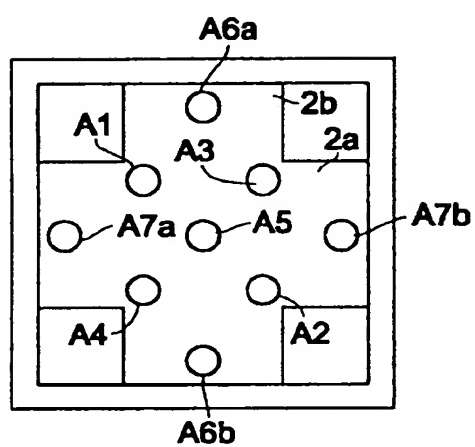


Fig. 3

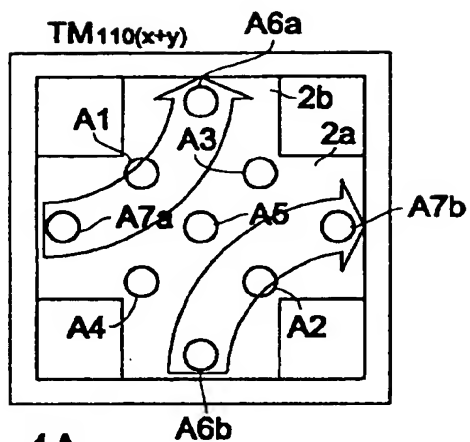


Fig. 4A

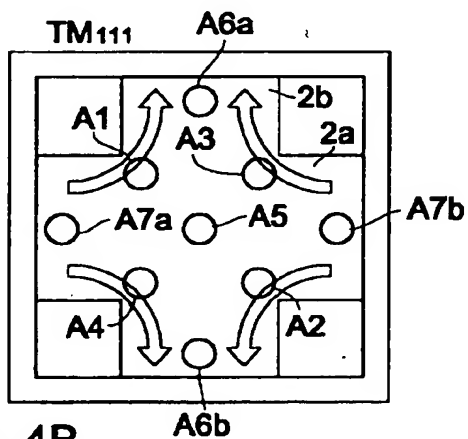


Fig. 4B

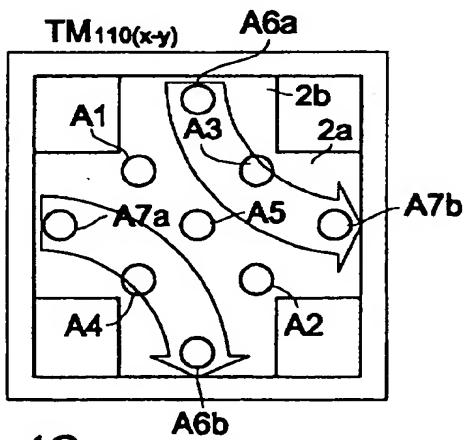


Fig. 4C

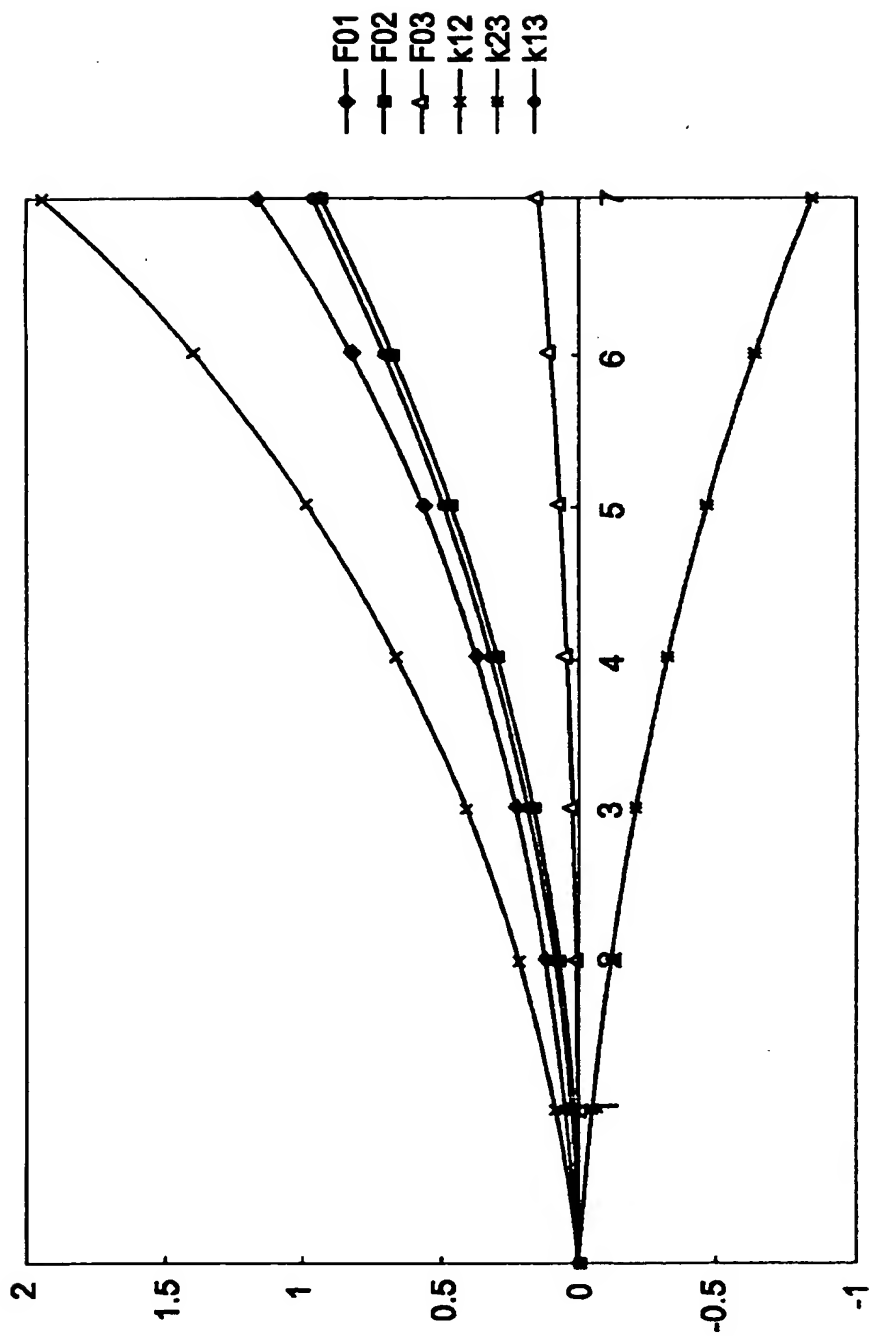


Fig. 5

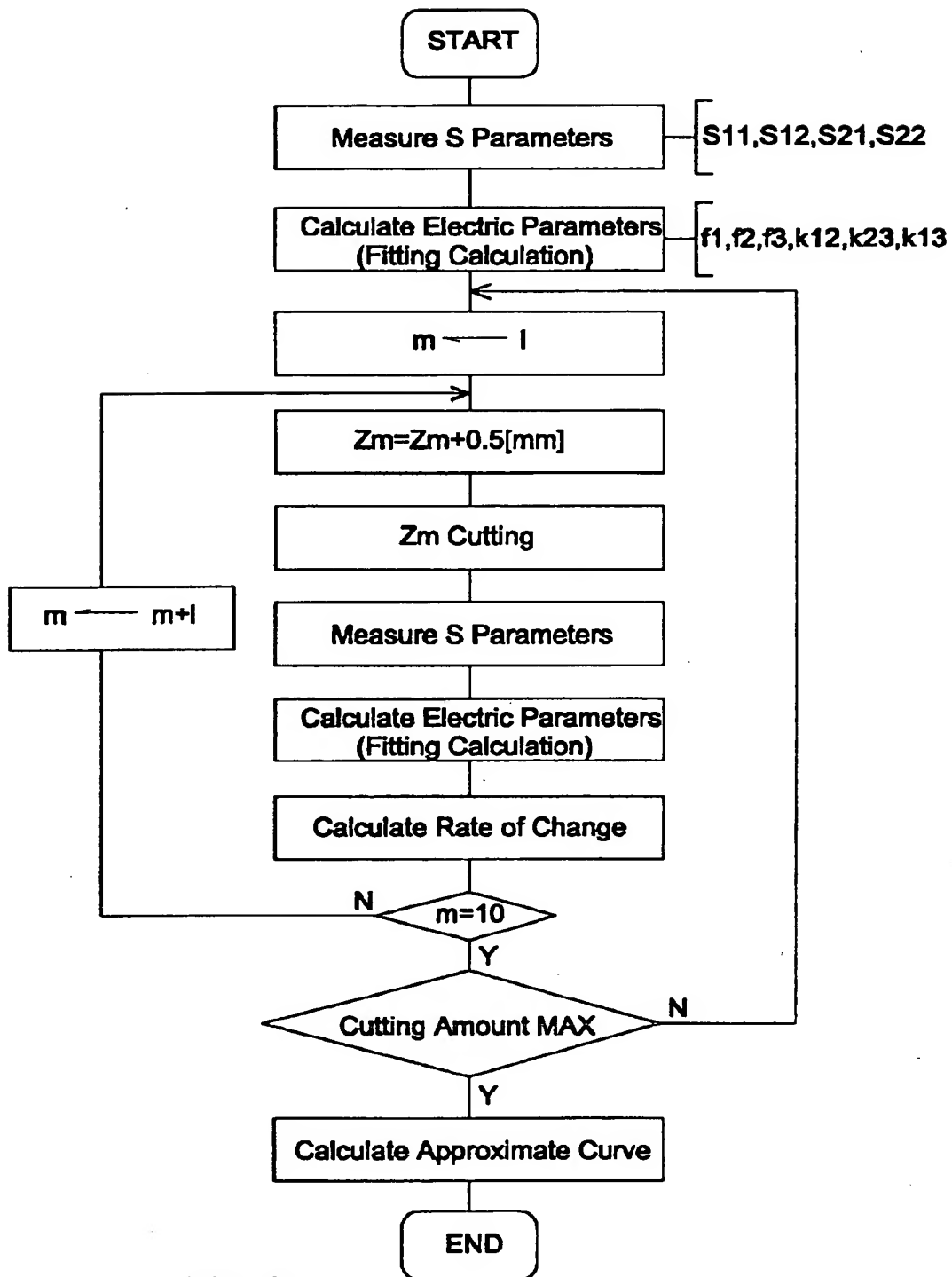


Fig. 6

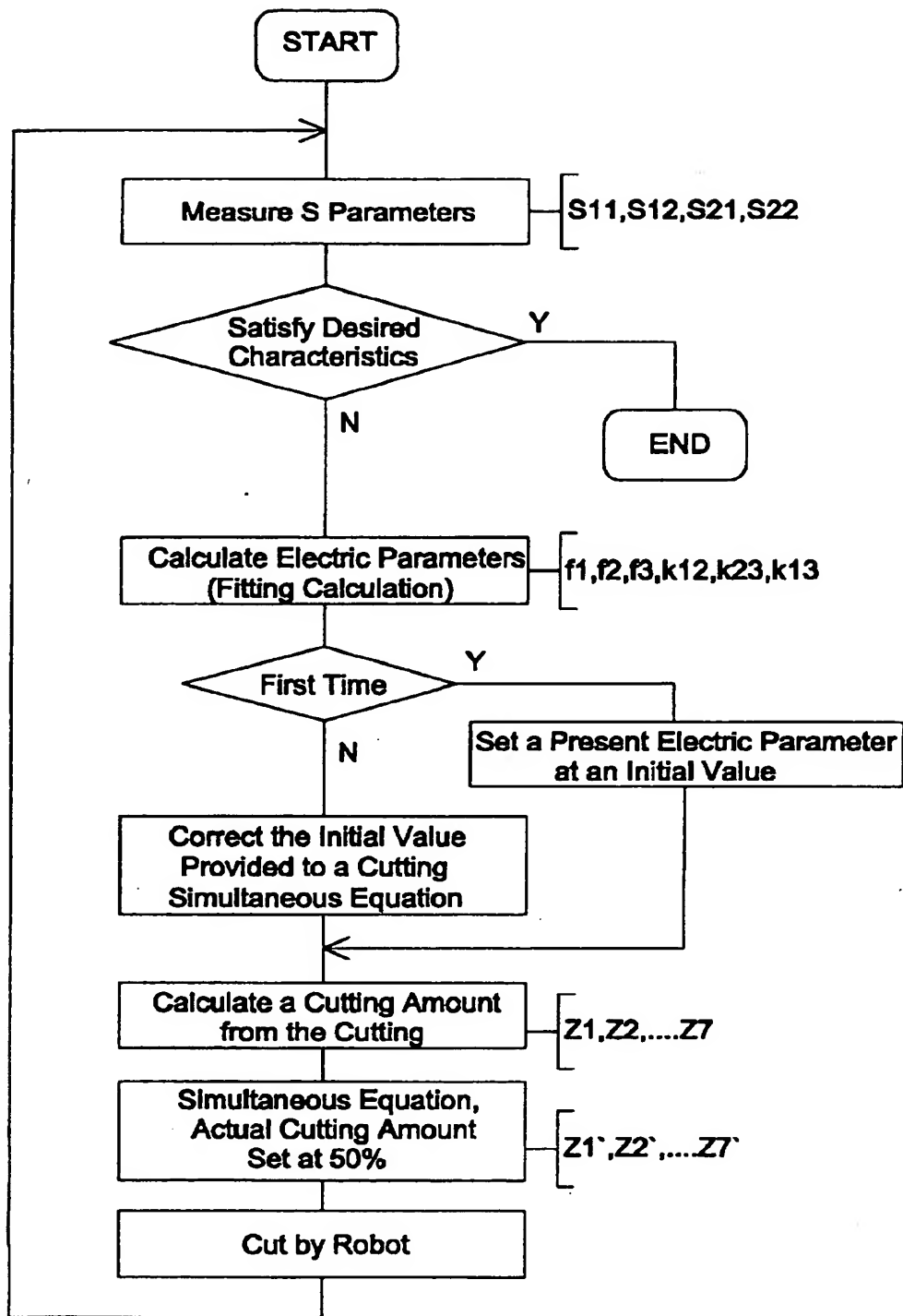


Fig. 7

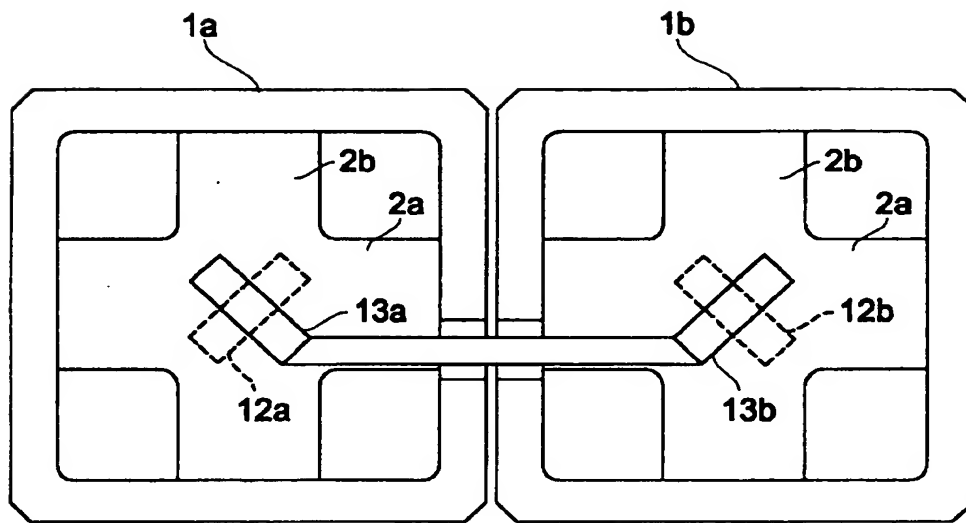


Fig. 8A

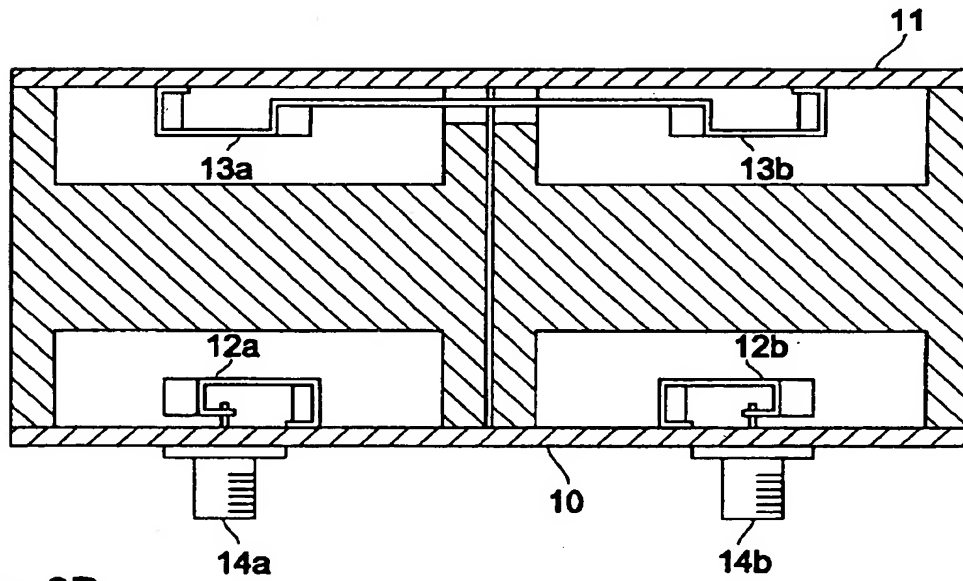


Fig. 8B

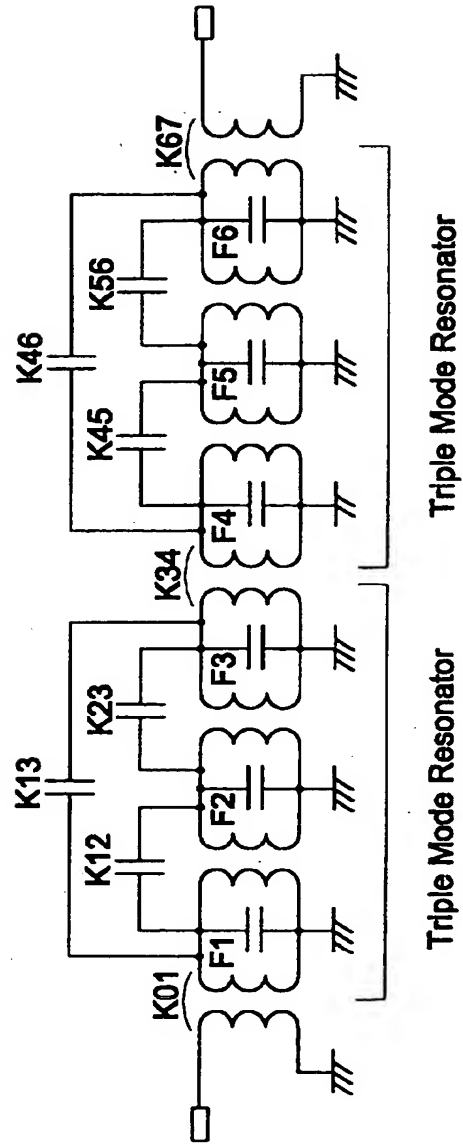


Fig. 9

Designed Parameter	Explanation	Resonator 1	Resonator 2
F1	Frequency of the First Stage	f1	-
F2	Frequency of the Second Stage	f2	-
F3	Frequency of the Third Stage	f3	-
F4	Frequency of the Fourth Stage	-	f1
F5	Frequency of the Fifth Stage	-	f2
F6	Frequency of the Sixth Stage	-	f3
K01	Combination Coefficient between an Input Loop and the First Stage	-	-
K12	Combination Coefficient between the First Stage and the Second Stage	k12	-
K23	Combination Coefficient between the Second Stage and the Third Stage	k23	-
K34	Combination Coefficient between the Third Stage and the Fourth Stage Combination Coefficient by virtue of a Combination Loop	-	-
K45	Combination Coefficient between the Fourth Stage and the Fifth Stage	-	k12
K56	Combination Coefficient between the Fifth Stage and the Sixth Stage	-	k23
K67	Combination Coefficient between the Sixth Stage and the Output Loop	-	-
K03	Combination Coefficient between the Input Loop and the Third Stage	-	-
K13	Combination Coefficient between the First Stage and the Third Stage	k13	-
K46	Combination Coefficient between the Fourth Stage and the Sixth Stage	-	k13
K47	Combination Coefficient between the Fourth Stage and the Output Loop	-	-
K07	Combination Coefficient between the Input Loop and the Output Loop	-	-
Q1	Q of the First Stage	f1@Q	-
Q2	Q of the Second Stage	f2@Q	-
Q3	Q of the Third Stage	f3@Q	-
Q4	Q of the Fourth Stage	-	f1@Q
Q5	Q of the Fifth Stage	-	f2@Q
Q6	Q of the Sixth Stage	-	f3@Q

Fig. 10



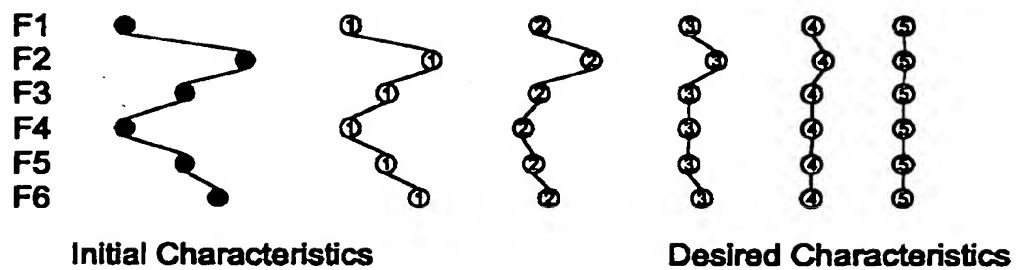


Fig. 11

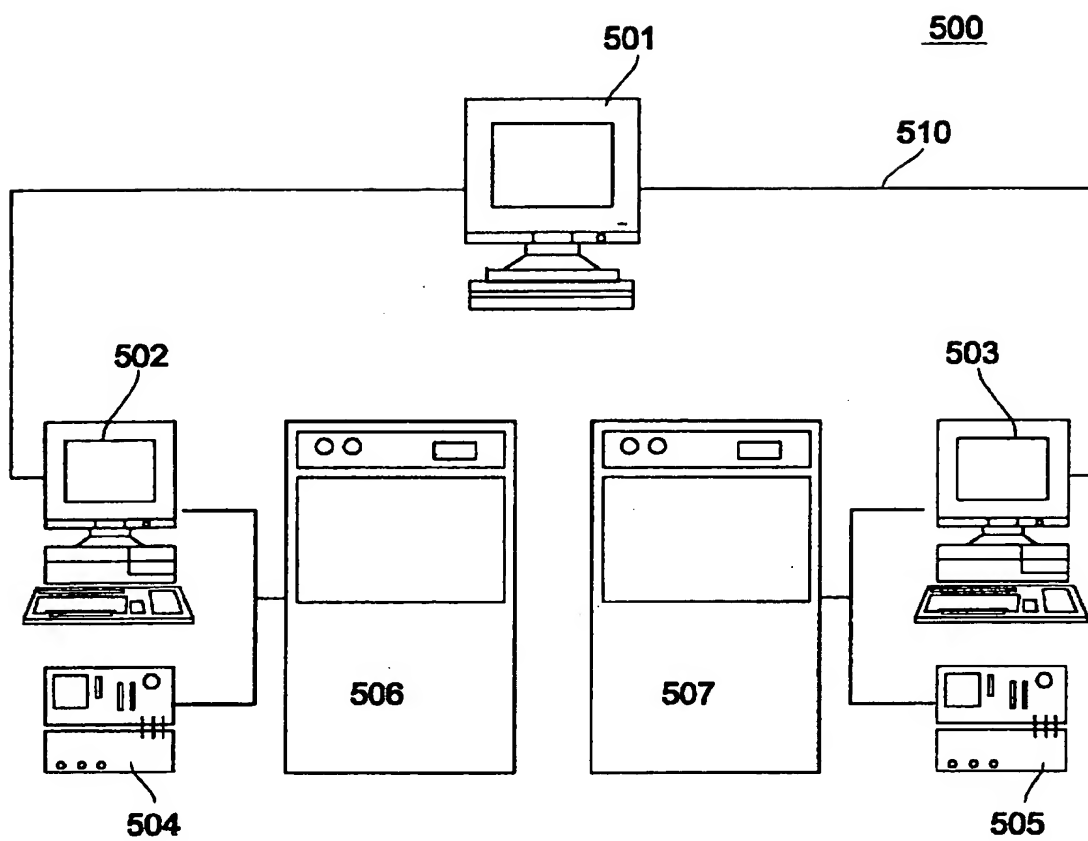


Fig. 12